

Ambiguity Function Shaping in FMCW Automotive Radar

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Abstract—Frequency-modulated continuous wave (FMCW) radar with inter-chirp coding produces high side-lobes in the Doppler and range dimensions of the radar’s ambiguity function. The high side-lobes may cause miss-detection due to masking between targets that are at similar range and have large received power difference, as is often the case in automotive scenarios. In this paper, we develop a novel code optimization method that attenuates the side-lobes of the radar’s ambiguity function. In particular, we introduce a framework for designing radar transmit sequences by shaping the radar Ambiguity Function (AF) to a desired structure. The proposed approach suppresses the average amplitude of the AF of the transmitted signal in regions of interest by efficiently tackling a longstanding optimization problem. The optimization criterion is quartic in nature with respect to the radar transmit code. A cyclic iterative algorithm is introduced that recasts the quartic problem as a unimodular quadratic problem (UQP) which can be tackled using power-method-like iterations (PMLI). Our numerical results demonstrate the effectiveness of the proposed algorithm in designing sequences with desired AF which is of great interest to the future generations of automotive radar sensors.

Index Terms—Ambiguity function, automotive radar, FMCW, power-method-like iterations, unimodular quadratic programming

I. INTRODUCTION

In radar signal processing, the range-Doppler response of the transmitted waveform also known as the ambiguity function plays a critical role, as it governs the Doppler and range resolutions of the system and regulates the interference power from unwanted returns at the output of the matched filter to the target signature. To put it another way, the radar designer is faced with the problem of choosing signal waveforms that yield desirable ambiguity functions. What is considered desirable, of course, depends on the operational use of the radar. While ambiguity function shaping is widely studied in the literature, the topic remains unexplored in the context of automotive radar [1].

In this paper, we study the ambiguity function shaping in frequency-modulated continuous wave (FMCW) automotive radar. Shaping radar ambiguity functions has long been considered difficult from a pure design or computational perspective due to the fact that the two-dimensional nature of the ambiguity function implies the number of design constraints would grow much faster than the design variables and that the design objective (to be optimized) has a quartic nature [2]. In [2], a

method based on maximum block improvement is devised to tackle the quartic objective in the ambiguity function shaping problem. In a more recent work in [3], an algorithm based on accelerated iterative sequential optimization is proposed to minimize the weighted integrated sidelobes level (WISL) over desired range-Doppler bins of interest. A similar problem is solved by successive application of majorization minimization (MM) and projected gradient descent algorithm (PGD) in [4]. This method can be inefficient due to the approximation error in the MM step. Similar problem is addressed by convex relaxation in [5].

In this paper, inspired by the algorithm proposed in [6], [7] for mutual interference mitigation, we devise a low-complexity algorithm based on power-method-like iterations to minimize the ambiguity function in the range-Doppler bins corresponding to echoes from clutters in the environment.

The rest of the paper is organized as follows. In the next section, we formulate the ambiguity function shaping problem for FMCW radar. In section III, we propose our algorithm for designing a radar code with the desired ambiguity function. We evaluate our method via numerical experiments in section IV and conclude the paper in section V.

Throughout this paper, we use bold lowercase and bold uppercase letters for vectors and matrices, respectively. \mathbb{R} represents the set of real numbers. $(\cdot)^\top$ and $(\cdot)^H$ denote the vector/matrix transpose, and the Hermitian transpose, respectively. $\text{Diag}(\cdot)$ denotes the diagonalization operator that produces a diagonal matrix with the same diagonal entries as the entries of its vector argument. The mn -th element of the matrix \mathbf{B} is $\mathbf{B}[m, n]$. The minimum eigenvalue of the matrix \mathbf{B} is denoted by $\gamma_{\min}(\cdot)$, respectively. The real, imaginary, and angle/phase components of a complex number are $\text{Re}\{\cdot\}$, $\text{Im}(\cdot)$, and $\arg\{\cdot\}$, respectively. Finally, $\delta_{i,j}$ is the extension of Kronecker delta function with $\delta_{i,j} = 1$ if $i = j$ and $\delta_{i,j} = 0$, otherwise.

II. PROBLEM FORMULATION

We start by considering an FMCW automotive radar system whose frequency is swept linearly over a bandwidth B in a time duration T_c . The transmit signal with an intra-pulse code length N can be represented as

$$s(t) = \sum_{n=1}^N x_n u(t - nT_c), \quad 0 \leq t \leq T_c \quad (1)$$

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where $\mathbf{x} = [x_1, \dots, x_N]^\top \in \mathbb{C}^N$ is the slow-time sequence and the chirp is

$$u(t) = \frac{1}{\sqrt{T_c}} \exp(j(2\pi f_c t + \pi K t^2)) \text{rect}\left(\frac{t}{T_c}\right), \quad (2)$$

where $K = \frac{B}{T_c}$ is the chirp rate, and

$$\text{rect}(t) = \begin{cases} 1 & 0 \leq t \leq 1, \\ 0 & \text{otherwise.} \end{cases} \quad (3)$$

In order to keep constant transmit power over the N chirps, we constrain the code sequence to be unimodular i.e. $|x_n| = 1$, for $n = 1, \dots, N$ [8], [9].

The ambiguity function is defined as [10],

$$\begin{aligned} \chi(\tau, \nu) &= \int_{-\infty}^{\infty} s(t) s^*(t - \tau) \exp(-j2\pi\nu(t - \tau)) dt \\ &= \int_0^T \left(\sum_{n=1}^N x_n u(t - nT_c) \right) \left(\sum_{m=1}^N x_m^* u^*(t - mT_c - \tau) \right) \\ &\quad \cdot \exp(-j2\pi\nu(t - \tau)) dt \\ &= \sum_{m=1}^N \sum_{n=1}^N x_m^* \left(\int_0^T u(t - nT_c) u^*(t - mT_c - \tau) e^{-j2\pi\nu(t - \tau)} dt \right) x_n. \end{aligned} \quad (4)$$

where τ is the time delay and ν is the Doppler frequency shift. With an aim to discretize the AF in (4), by setting $\tau = kT_c$ for $k = -N + 1, \dots, 0, \dots, N - 1$ and $\nu = \frac{p}{NT_c}$ for $p = -\frac{N}{2}, \dots, \frac{N}{2} - 1$ for even p or $p = -\frac{N-1}{2}, \dots, \frac{N-1}{2}$ for odd p , we can easily obtain,

$$\begin{aligned} \chi[k, p] &\triangleq \chi(kT_c, \frac{p}{NT_c}) \\ &= e^{j\pi \frac{p}{N}} \text{sinc}\left(\pi \frac{p}{N}\right) \sum_{n=1}^N x_n x_{n-k}^* e^{-j\pi(n-k)p/N}. \end{aligned} \quad (5)$$

where $\text{sinc}(x) = \sin(x)/x$. We assume the target under study is moving with low speed i.e. $|\nu| \ll 1/T_c$. Therefore, it is safe to confine our attention to values of $|p| \ll N$ in which case $\text{sinc}\left(\pi \frac{p}{N}\right) \approx 1$ and thus the discrete-AF can be defined as,

$$r[k, p] \triangleq \sum_{n=1}^N x_n x_{n-k}^* e^{-j2\pi \frac{(n-k)p}{N}}. \quad (6)$$

for $k = -N + 1, \dots, 0, \dots, N - 1$ and $p = -\frac{N}{2}, \dots, \frac{N}{2} - 1$ for even p or $p = -\frac{N-1}{2}, \dots, \frac{N-1}{2}$ for odd p . In the next section, we will primarily be focused on designing the sequence $\{x_n\}_{n=1}^N$ so as to minimize the sidelobes of the discrete-AF in a certain region.

III. PROPOSED METHOD

The goal herein is to suppress the energy of the discrete-AF in a region of interest defined by the index sets \mathcal{K}, \mathcal{P} for delay and Doppler shift, respectively, by minimizing the criterion:

$$C = \sum_{k \in \mathcal{K}} \sum_{p \in \mathcal{P}} |r[k, p]|^2. \quad (7)$$

In particular, the AF shaping problem that we are interested in is

$$\begin{aligned} \mathcal{M}_1 : \text{minimize}_{\mathbf{x}} \quad & C \\ \text{s.t. } \mathbf{x} \text{ is } & \text{unimodular.} \end{aligned} \quad (8)$$

Note that the discrete-AF $r[k, p]$ can be reformulated as

$$r[k, p] = \mathbf{x}^H \mathbf{D}_p \mathbf{J}_k \mathbf{x}, \quad (9)$$

where

$$\mathbf{D}_p = \text{Diag}\left(\left[e^{-j2\pi \frac{p}{N}}, \dots, e^{-j2\pi \frac{(N-1)p}{N}}, e^{-j2\pi \frac{Np}{N}}\right]\right), \quad (10)$$

and

$$\mathbf{J}_k = \mathbf{J}_{-k}^H = \begin{bmatrix} \mathbf{0} & \mathbf{I}_{N-k} \\ \mathbf{I}_k & \mathbf{0} \end{bmatrix} \quad (11)$$

is the shift matrix that performs the shifting of the vector being multiplied by k lags. Therefore the problem in (7) can be recast as,

$$\begin{aligned} C &= \sum_{k \in \mathcal{K}} \sum_{p \in \mathcal{P}} |\mathbf{x}^H \mathbf{D}_p \mathbf{J}_k \mathbf{x}|^2 \\ &= \sum_{k \in \mathcal{K}} \sum_{p \in \mathcal{P}} |\mathbf{x}^H \mathbf{A}_{k,p} \mathbf{x}|^2 \end{aligned} \quad (12)$$

where $\mathbf{A}_{k,p} = \mathbf{D}_p \mathbf{J}_k$. Interestingly, as one can observe, C is quartic with respect to \mathbf{x} making \mathcal{M}_1 in (8) a non-convex problem. In order to recast the problem in a quadratic form, let

$$\begin{aligned} \mathbf{A}_{k,p}^r &\triangleq \frac{1}{2} (\mathbf{A}_{k,p} + \mathbf{A}_{k,p}^H), \\ \mathbf{A}_{k,p}^i &\triangleq \frac{1}{2} (\mathbf{A}_{k,p} - \mathbf{A}_{k,p}^H) \end{aligned} \quad (13)$$

and note that

- 1) Matrices $\mathbf{A}_{k,p}^r$ and $j\mathbf{A}_{k,p}^i$ are Hermitian and skew-Hermitian matrices, respectively [11].
- 2) For any generic vector \mathbf{z} ,

$$\mathbf{z}^H \mathbf{A}_{k,p} \mathbf{z} = \mathbf{z}^H \mathbf{A}_{k,p}^r \mathbf{z} + \mathbf{z}^H \mathbf{A}_{k,p}^i \mathbf{z} \quad (14)$$

where

$$\mathbf{z}^H \mathbf{A}_{k,p}^r \mathbf{z} \in \mathbb{R} \quad \text{and} \quad j\mathbf{z}^H \mathbf{A}_{k,p}^i \mathbf{z} \in \mathbb{R}. \quad (15)$$

In particular, it follows from (15) that

$$|\mathbf{z}^H \mathbf{A}_{k,p} \mathbf{z}|^2 = |\mathbf{z}^H \mathbf{A}_{k,p}^r \mathbf{z}|^2 + |\mathbf{z}^H j\mathbf{A}_{k,p}^i \mathbf{z}|^2. \quad (16)$$

Hence we can write,

$$\begin{aligned} \sum_{k,p} |\mathbf{x}^H \mathbf{A}_{k,p} \mathbf{x}|^2 &= \sum_{k,p} |\mathbf{x}^H \mathbf{A}_{k,p}^r \mathbf{x}|^2 + |\mathbf{x}^H j\mathbf{A}_{k,p}^i \mathbf{x}|^2 \\ &= \sum_{k,p} |\mathbf{x}^H (\mathbf{A}_{k,p}^r + \zeta \mathbf{I}_N) \mathbf{x} - \zeta N|^2 \\ &\quad + |\mathbf{x}^H (j\mathbf{A}_{k,p}^i + \zeta \mathbf{I}_N) \mathbf{x} - \zeta N|^2 \\ &= \sum_{k,p} |\mathbf{x}^H \tilde{\mathbf{A}}_{k,p}^r \mathbf{x} - \zeta N|^2 + |\mathbf{x}^H \tilde{\mathbf{A}}_{k,p}^i \mathbf{x} - \zeta N|^2 \end{aligned} \quad (17)$$

where

$$\tilde{\mathbf{A}}_{k,p}^r = \mathbf{A}_{k,p}^r + \zeta \mathbf{I}_N, \quad (18)$$

$$\tilde{\mathbf{A}}_{k,p}^i = j\mathbf{A}_{k,p}^i + \zeta \mathbf{I}_N \quad (19)$$

and $\zeta \in \mathbb{R}$ is chosen such that

$$\zeta > -\min \left(\bigcup_{k,p} \{ \gamma_{\min}(\mathbf{A}_{k,p}^r), \gamma_{\min}(j\mathbf{A}_{k,p}^i) \} \right). \quad (20)$$

The modification in (18)-(19) is known as diagonal loading and it ensures the positive definiteness of $\{\tilde{\mathbf{A}}_{k,p}^r\}$ and $\{\tilde{\mathbf{A}}_{k,p}^i\}$. The objective (17) is still quartic w.r.t. \mathbf{x} . In order to make it quadratic we resort to the equivalence properties of Hermitian square roots.

Remark 1. For the positive definite matrix $\tilde{\mathbf{A}}_{k,p}^r$, $\mathbf{x}^H \tilde{\mathbf{A}}_{k,p}^r \mathbf{x}$ is close to ζN , if and only if $(\tilde{\mathbf{A}}_{k,p}^r)^{1/2} \mathbf{x}$ is close to $\sqrt{\zeta N} \mathbf{u}_{k,p}^r$, for a unit-norm vector $\mathbf{u}_{k,p}^r$. Similarly, $\mathbf{x}^H \tilde{\mathbf{A}}_{k,p}^i \mathbf{x}$ is close to ζN , if and only if $(\tilde{\mathbf{A}}_{k,p}^i)^{1/2} \mathbf{x}$ is close to $\sqrt{\zeta N} \mathbf{u}_{k,p}^i$, for a unit-norm vector $\mathbf{u}_{k,p}^i$ [11].

According to Remark 1, \mathcal{M}_1 is equivalent to

$$\begin{aligned} \mathcal{M}_2 : \quad & \underset{\mathbf{x}, \{\mathbf{u}_{k,p}^r\}, \{\mathbf{u}_{k,p}^i\}}{\text{minimize}} \quad \sum_{k,p} \left\{ \left\| (\tilde{\mathbf{A}}_{k,p}^r)^{1/2} \mathbf{x} - \sqrt{\zeta N} \mathbf{u}_{k,p}^r \right\|_2^2 \right. \\ & \left. + \left\| (\tilde{\mathbf{A}}_{k,p}^i)^{1/2} \mathbf{x} - \sqrt{\zeta N} \mathbf{u}_{k,p}^i \right\|_2^2 \right\} \\ & \text{s.t. } \mathbf{x} \text{ is unimodular,} \\ & \|\mathbf{u}_{k,p}^r\|_2 = \|\mathbf{u}_{k,p}^i\|_2 = 1 \text{ for all } k \in \mathcal{K}, p \in \mathcal{P}, \end{aligned} \quad (21)$$

which is quadratic w.r.t. \mathbf{x} , $\{\mathbf{u}_{k,p}^r\}$ and $\{\mathbf{u}_{k,p}^i\}$ and equivalent to \mathcal{M}_1 in (8). In the following, we follow a cyclic optimization approach to tackle the problem (8) in an alternating manner over \mathbf{x} , $\{\mathbf{u}_{k,p}^r\}$ and $\{\mathbf{u}_{k,p}^i\}$.

A. Optimization w.r.t. \mathbf{x}

The objective function in \mathcal{M}_2 is recast as

$$\begin{aligned} C_{\mathbf{x}} = \mathbf{x}^H & \left(\sum_{k,p} \left(\tilde{\mathbf{A}}_{k,p}^r + \tilde{\mathbf{A}}_{k,p}^i \right) \right) \mathbf{x} \\ & - 2\sqrt{\zeta N} \operatorname{Re} \left\{ \mathbf{x}^H \sum_{k,p} \left(\tilde{\mathbf{A}}_{k,p}^r \right)^{H/2} \mathbf{u}_{k,p}^r \right\} \\ & - 2\sqrt{\zeta N} \operatorname{Re} \left\{ \mathbf{x}^H \sum_{k,p} \left(\tilde{\mathbf{A}}_{k,p}^i \right)^{H/2} \mathbf{u}_{k,p}^i \right\} + \text{const.} \end{aligned} \quad (22)$$

Or simply,

$$C_{\mathbf{x}} = \mathbf{x}^H \mathbf{R} \mathbf{x} + 2 \operatorname{Re} \{ \mathbf{x}^H \mathbf{s}_{\mathbf{x}} \} + \text{const.} \quad (23)$$

where

$$\mathbf{R} = \sum_{k,p} \left(\tilde{\mathbf{A}}_{k,p}^r + \tilde{\mathbf{A}}_{k,p}^i \right) \quad (24)$$

and

$$\mathbf{s}_{\mathbf{x}} = -\sqrt{\zeta N} \sum_{k,p} \left(\left(\tilde{\mathbf{A}}_{k,p}^r \right)^{H/2} \mathbf{u}_{k,p}^r + \left(\tilde{\mathbf{A}}_{k,p}^i \right)^{H/2} \mathbf{u}_{k,p}^i \right) \quad (25)$$

By dropping the constant term, the objective function can be reformulated as,

$$\begin{aligned} C_{\mathbf{x}} &= \mathbf{x}^H \mathbf{R} \mathbf{x} + 2 \operatorname{Re} \{ \mathbf{x}^H \mathbf{s}_{\mathbf{x}} \} \\ &= \begin{bmatrix} \mathbf{x} \\ 1 \end{bmatrix}^H \begin{bmatrix} \mathbf{R} & \mathbf{s}_{\mathbf{x}} \\ \mathbf{s}_{\mathbf{x}}^H & 0 \end{bmatrix} \begin{bmatrix} \mathbf{x} \\ 1 \end{bmatrix} \\ &= \bar{\mathbf{x}}^H \mathbf{B}_{\mathbf{x}} \bar{\mathbf{x}} \end{aligned} \quad (26)$$

Hence, \mathcal{M}_2 w.r.t \mathbf{x} is equivalent to

$$\begin{aligned} & \underset{\bar{\mathbf{x}}}{\text{minimize}} \quad \bar{\mathbf{x}}^H \mathbf{B}_{\mathbf{x}} \bar{\mathbf{x}} \\ & \text{s.t. } |x_n| = 1, \quad n = 1, \dots, N, \\ & \bar{\mathbf{x}} = \begin{bmatrix} \mathbf{x} \\ 1 \end{bmatrix}. \end{aligned} \quad (27)$$

We perform diagonal loading on $\mathbf{B}_{\mathbf{x}}$ to obtain the equivalent problem

$$\begin{aligned} & \underset{\bar{\mathbf{x}}}{\text{maximize}} \quad \bar{\mathbf{x}}^H \mathbf{D}_{\mathbf{x}} \bar{\mathbf{x}} \\ & \text{s.t. } |x_n| = 1, \quad n = 1, \dots, N, \\ & \bar{\mathbf{x}} = \begin{bmatrix} \mathbf{x} \\ 1 \end{bmatrix}. \end{aligned} \quad (28)$$

where $\mathbf{D}_{\mathbf{x}} \triangleq \gamma_{\mathbf{x}} \mathbf{I}_{(N+1)} - \mathbf{B}_{\mathbf{x}}$, with $\gamma_{\mathbf{x}}$ being larger than the maximum eigenvalue of $\mathbf{B}_{\mathbf{x}}$. The above problem is called unimodular quadratic programming (UQP) and the power-method-like iterations,

$$\mathbf{x}^{(t,s+1)} = \exp \left\{ j \arg \left\{ \begin{bmatrix} \mathbf{I}_{N \times N} \\ \mathbf{0}_{1 \times N} \end{bmatrix}^T \mathbf{D}_{\mathbf{x}} \bar{\mathbf{x}}^{(t,s)} \right\} \right\} \quad (29)$$

introduced in [12] leads to a monotonically decreasing objective value for UQP. The iterations can be initialized with the latest design of \mathbf{x} denoted by $\mathbf{x}^{(t,0)}$, where t denotes the iteration number as we see later in Algorithm 1.

B. Optimization w.r.t. $\{\mathbf{u}_{k,p}^r\}$ and $\{\mathbf{u}_{k,p}^i\}$

Using (22), the problem \mathcal{M}_2 w.r.t $\mathbf{u}_{k,p}^r$ is equivalent to

$$\begin{aligned} & \underset{\mathbf{u}_{k,p}^r}{\text{minimize}} \quad \operatorname{Re} \left\{ \mathbf{x}^H \left(\tilde{\mathbf{A}}_{k,p}^r \right)^{H/2} \mathbf{u}_{k,p}^r \right\} \\ & \text{s.t. } \|\mathbf{u}_{k,p}^r\|_2 = 1. \end{aligned} \quad (30)$$

Therefore, we have the closed-form solution for $\mathbf{u}_{k,p}^r$ as

$$\hat{\mathbf{u}}_{k,p}^r(t) = \frac{\left(\tilde{\mathbf{A}}_{k,p}^r \right)^{1/2} \mathbf{x}}{\left\| \left(\tilde{\mathbf{A}}_{k,p}^r \right)^{1/2} \mathbf{x} \right\|_2}, \quad (31)$$

where t is the iteration number as used in Algorithm 1. A similar closed-form solution works mutatis mutandis for $\mathbf{u}_{k,p}^i$ as

$$\hat{\mathbf{u}}_{k,p}^i(t) = \frac{\left(\tilde{\mathbf{A}}_{k,p}^i \right)^{1/2} \mathbf{x}}{\left\| \left(\tilde{\mathbf{A}}_{k,p}^i \right)^{1/2} \mathbf{x} \right\|_2}. \quad (32)$$

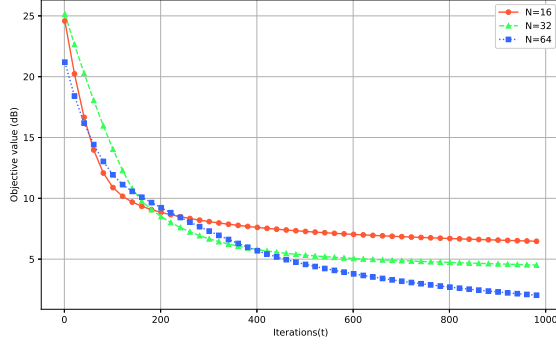


Figure 1. The objective value in (7) versus the iterations of Algorithm 1

At each cycle of the algorithm, we compute (31)-(32) corresponding to each $k \in \mathcal{K}$ and $p \in \mathcal{P}$. The final algorithm consisting of iterations over (29) and (31)-(32) is summarized in Algorithm 1. The number of outer iterations, Γ_1 , in the algorithm is chosen such that $|(C^{(t+1)} - C^{(t)})/C^{(t)}| \leq \epsilon$, where $C^{(t)}$ is the objective value introduced in (7), is satisfied at the final iteration. Similarly, the number of inner iterations Γ_2 is chosen such that the power method like iterations in (29) for updating \mathbf{x} converges in terms of changes in objective value.

Algorithm 1 Radar code design for shaping the ambiguity function

Input: Index sets \mathcal{K} and \mathcal{P} , $\mathbf{x}^{(0,0)}$, $\mathbf{u}_{k,p}^{r(0)}$, $\mathbf{u}_{k,p}^{i(0)}$ for $k \in \mathcal{K}$ and $p \in \mathcal{P}$, Γ_1, Γ_2 .

Output: \mathbf{x}

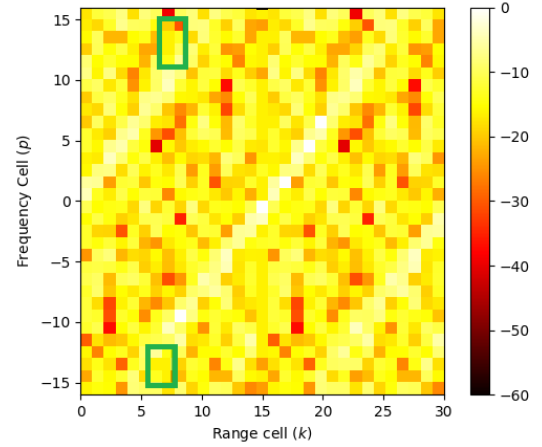
- 1: **for** $t = 0 : \Gamma_1 - 1$ **do**
- 2: **for** $s = 0 : \Gamma_2 - 1$ **do**
- 3: Update \mathbf{D}_x by plugging in $\hat{\mathbf{u}}_{k,p}^{r(t)}$ and $\hat{\mathbf{u}}_{k,p}^{i(t)}$ in (25)-(28).
- 4: $\mathbf{x}^{(t,s+1)} \leftarrow \exp \left\{ j \arg \left\{ \begin{bmatrix} \mathbf{I}_{N \times N} \\ \mathbf{0}_{1 \times N} \end{bmatrix}^T \mathbf{D}_x \bar{\mathbf{x}}^{(t,s)} \right\} \right\}$
- 5: $\hat{\mathbf{u}}_{k,p}^{r(t+1)} \leftarrow \frac{(\tilde{\mathbf{A}}_{k,p}^r)^{1/2} \mathbf{x}^{(t,s)}}{\|(\tilde{\mathbf{A}}_{k,p}^r)^{1/2} \mathbf{x}^{(t,s)}\|_2}$, $k \in \mathcal{K}$ and $p \in \mathcal{P}$.
- 6: $\hat{\mathbf{u}}_{k,p}^{i(t+1)} \leftarrow \frac{(\tilde{\mathbf{A}}_{k,p}^i)^{1/2} \mathbf{x}^{(t,s)}}{\|(\tilde{\mathbf{A}}_{k,p}^i)^{1/2} \mathbf{x}^{(t,s)}\|_2}$, $k \in \mathcal{K}$ and $p \in \mathcal{P}$.
- 7: $\hat{\mathbf{u}}_{k,p}^{i(t+1)} \leftarrow \frac{(\tilde{\mathbf{A}}_{k,p}^i)^{1/2} \mathbf{x}^{(t,s)}}{\|(\tilde{\mathbf{A}}_{k,p}^i)^{1/2} \mathbf{x}^{(t,s)}\|_2}$, $k \in \mathcal{K}$ and $p \in \mathcal{P}$.
- 8: **return** $\mathbf{x} \leftarrow \mathbf{x}^{(\Gamma_1, \Gamma_2)}$

IV. NUMERICAL EXPERIMENTS

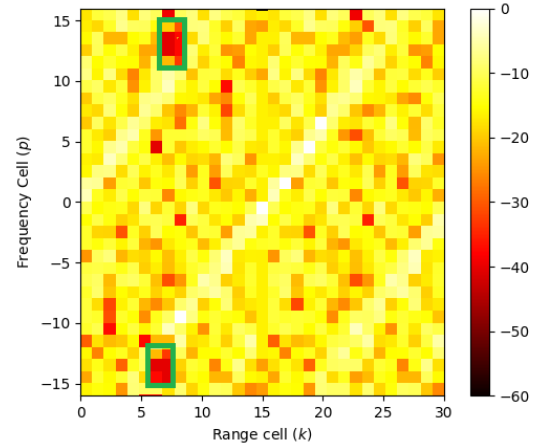
In this section, we will examine the capability of Algorithm 1 which has been proposed to design a radar phase code that has an ambiguity function with the desired shape. The region of interest is defined by the sets \mathcal{K} and \mathcal{P} as

$$\begin{aligned} \mathcal{K} &= \{5, 6, 7\} \quad \text{and} \\ \mathcal{P} &= \{-15, -14, -13, 11, 12, 13, 14\}. \end{aligned} \quad (33)$$

A random phase-code unimodular sequence of length $N = 31$ is generated as the starting sequence for the algorithm.



(a)



(b)

Figure 2. Ambiguity function, in dB, of (a) the initial random code and (b) the synthesized FMCW code with $N = 16$ and in green the assumed regions of interest.

Moreover, we execute the UQP subroutine for $\Gamma_2 = 500$ times and allow for at most $\Gamma_1 = 10^3$ runs of the outer iterations. As illustrated in Fig. 2, the radar code synthesized by algorithm 1 has the desired ambiguity function values in the chosen bins corresponding to interference.

V. SUMMARY

In this paper, we addressed the unimodular radar code design for FMCW radar ambiguity function shaping. We devised the radar codes by minimizing a criterion obtained from the absolute value of the ambiguity function in the regions of interest and we addressed the quartic optimization problem using the PMLI iterations. Numerical experiments were conducted to demonstrate the efficacy of the proposed method in shaping the ambiguity function.

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